The Oxidation of 2,4,6-trinitroresorcine (TNR) using zero-valent iron (ZVI)

Le Quoc Trung\textsuperscript{a}, Nguyen Duc Hung\textsuperscript{a}, Tran Van Chung\textsuperscript{a}, I. Francis Cheng\textsuperscript{b}

\textsuperscript{a} Institute of Chemicals and Materials, Hanoi Vietnam
\textsuperscript{b} Department of Chemistry, University of Idaho, Moscow, Idaho 83844-23-43

Abstract

This paper describes the character of the reduction of TNR by ZVI in anaerobic conditions and the oxidative reaction of amine resorcine in the system of ZVI-EDTA-O\textsubscript{2}. The products of TNR by ZVI in anaerobic conditions were amine resorcine compounds. These compounds tend to be easier to oxidize by the free radical OH\textsuperscript{-} generated in the system of ZVI-EDTA-O\textsubscript{2}. HPLC and Chemical Oxygen Demand analysis (COD) were used to monitor the efficiency of reactions. The experiments have suggested that the removal of TNR from groundwater should be implemented by a two step process. The first step is reduction of TNR by ZVI to form amine resorcine. The second step is oxidation of amine resorcine in system consisting of ZVI-EDTA-O\textsubscript{2}. From the obtained results a model for TNR contaminated groundwater treatment has been suggested and tested.

Keywords: Reduction of TNR, Two step removal of TNR, Treatment of TNR, Zero-valent iron with TNR

Introduction

Groundwater contamination has become a serious problem. Explosive chemicals such as 2,4,6-trinitrotoluene (TNT), 2,4,6-trinitroresorcine (TNR), hexahydro-1,3,5-trinitro-1,3,5-triazine (RDX) disposed from monitions manufacturing plants and weapons testing areas have been a critical environmental problem. These compounds are highly stable in the environment and are somewhat soluble causing the toxicity to aquatic animals. They are also toxic to humans and can cause a host of health problems such as anemia and liver dysfunction. The EPA classifies them as a group C carcinogen.

The TNT, TNR, RDX may be removed from groundwater by such methods as adsorption onto granular activated carbon, destruction by photo catalysis, biodegradation and incineration. Recently ZVI particles have been used for treatment of many recalcitrant organic compounds like nitro aromatic, chlorinated compounds [1, 2, 3]. The chemical background of this method consists of the following reactions:
In the absence of oxygen, we have

\[ \text{Fe}^{(0)} \rightarrow \text{Fe}^{2+} + 2e^- \quad (1) \]
\[ \text{Fe}^{2+} \rightarrow \text{Fe}^{3+} + \text{1e}^- \quad (2) \]
\[ 2\text{H}_2\text{O} + 2e^- \rightarrow \text{H}_2(\text{g}) + \text{OH}^- \quad (3) \]

In principle, \( \text{Fe}^{(0)} \), \( \text{Fe}^{2+} \) and \( \text{H}_2 \) (little) can contribute to the reduction of contaminants [4]. The predominant degradation pathway for chlorinated compounds (RX) and for nitroaromatic compounds (ArNO\(_2\)) appears to be reductive processes:

\[ \text{RX} + \text{H}^+ + 2e^- \rightarrow \text{RH} + \text{X}^- \quad (4) \]
\[ \text{ArNO}_2 + 6e^- + 6 \text{H}^+ \rightarrow \text{ArNH}_2 + 2 \text{H}_2\text{O} \quad (5) \]

The reduced products such as \( \text{RH} \), \( \text{ArNH}_2 \) may be easy treated by biodegradation. The rates of reactions (4-5), depend on the factors such as size, surface area of ZVI particles, pH of solution, concentration of dissolved oxygen, carbonate ions, contaminant concentrations and some organic compounds, especially ethylenediaminetetraacetic acid (EDTA).

The system of \( \text{Fe}^{2+} - \text{H}_2\text{O} - \text{EDTA} \) in presence of oxygen has demonstrated such a strong oxidative character that it could mineralize many refractory organic compounds. The oxidative character of this system based on the following reactions, [5].

\[ 2\text{Fe}^{(0)} + \text{O}_2 + 2\text{H}_2\text{O} \rightarrow 2\text{Fe}^{2+} + 4\text{OH}^- \quad (6) \]
\[ \text{Fe}^{(II)}\text{EDTA} + \text{O}_2 \rightarrow \text{O}_2\text{Fe}^{(II)}\text{EDTA}, \quad k_1 = 10^3 \text{ M}^{-1}\text{s}^{-1} \quad (7) \]
\[ \text{O}_2\text{Fe}^{(II)}\text{EDTA} \rightarrow \text{Fe}^{(III)}\text{EDTA} + \text{O}_2^- \, , \quad k_2 = 10^2 \text{ M}^{-1}\text{s}^{-1} \quad (8) \]
\[ \text{Fe}^{(II)}\text{EDTA} + \text{O}_2^- \rightarrow \text{O}_2^{2-}\text{-Fe}^{(III)}\text{EDTA} \, , \quad k_3 = 10^6 \text{ M}^{-1}\text{s}^{-1} \quad (9) \]
\[ \text{O}_2^{2-}\text{-Fe}^{(III)}\text{EDTA} + 2\text{H}^+ \rightarrow \text{Fe}^{(III)}\text{EDTA} + \text{H}_2\text{O}_2 \, , \quad k_4 \text{ fast} \quad (10) \]
\[ \text{Fe}^{(II)}\text{EDTA} + \text{H}_2\text{O}_2 \rightarrow \text{Fe}^{(III)}\text{EDTA} + \text{OH}^- + \text{OH}^+ \, , \quad k_5 = 10^3 \text{ M}^{-1}\text{s}^{-1} \quad (11) \]

The \( \text{Fe}^{(II)}\text{EDTA} \) complex formed in the solution plays in role of catalyst for this conversion reaction. The free radical \( \text{OH}^+ \) plays the role of oxidative reagent in mineralization process.

In this paper we present the study on the mineralization of TNR from groundwater using zero-valent iron (ZVI) in presence of EDTA and oxygen. The experimental method was carried out by two steps: (i) reduction of TNR by ZVI under anaerobic conditions to result in amine products, (ii) oxidation of amine products in system consisting of ZVI, EDTA and oxygen. Focusing on the mineralization of TNR to be applied in environmental treatment, the efficiency of TNR mineralization has been exhibited by the variation of the COD during experiments.
Materials and Methods

Chemicals:

2,4,6-trinitroresorcine, zero-valent iron and ethylenediaminetetraacetic acid (EDTA) were obtained in high purity from Chem-Service, R.P, China, PA. The ZVI particles have trace impurities less than 0.02% C, 0.01% S, 0.002% Mn, 0.001% P. Prior to all experiments they must be treated by a HCl diluted acid to remove the oxide layer and other contaminants. ZVI pretreatment: Prior to use, the ZVI particles were hand-sieved to constrain grain size to 18-20 mesh and sonicated in HCl of 10% (v/v) for 20min. To remove the oxide layer and other contaminants. The clean metal was washed four times with bicarbonate buffer to avoid further surface oxidation to metal oxides. The BET surface area of the iron sample was between 3.5 to 4.5 m$^2$/g. The pH solution for all experiments was controlled by an acid or basic solution, H$_2$SO$_4$ 0.1M, NaOH 0.1M respectively.

Reduction of TNR by ZVI particles (step 1):

Batch experiments were conducted under anaerobic conditions in 500-ml round flask. The flask was spiked with 0.5 ml TNR stock solution and distilled water, to get a total volume of 250 ml with an initial concentration of 80mg/L, pH = 5.5, with the oxygen by N$_2$ purge. The TNR concentrations during the experiments were monitored by HPLC analysis. The sample for HPLC analysis was filtered through a 0.45 µm Nalgene 4 mm nylon filter (Fisher, Pittsburgh, PA) and TNR analyzed by HPLC with diode array detector with wavelength set 340nm. Analysis by HPLC was performed with a C-18 column (length 250mm, ID4.6mm; Altech, Deerfield, IL). The mobile phase used was a mixture of 45:55 acetonitrile/water with a flow rate of 1.0 ml/min. These experiments would allow us to determine the time when almost TNR conc. in the samples were reduced, converted into amine products.

Oxidation of amine products (step 2):

The amine products obtained from reduction of TNR by ZVI were filtered to removal iron particles for the further oxidation. Batch experiments were conducted under aerobic conditions in 500-ml open round flask. The flask contains the amine products (near 250ml solution). The flasks received 10g of dry, sieved iron and 84mg EDTA. Each reactor (flask) was placed on shaker with 40 rpm at room temperature. After every 30 minutes, a sample of 10ml was taken, filtered for measurement of chemical oxygen demand (COD). An analysis of COD was, then carried out by titrimetric method. The oxidation efficiency of TNR was calculated by the expression as follows:

$$E = \frac{[COD]_0 - [COD]_t}{[COD]_0} \times 100, \% \quad (1)$$

Here $[COD]_0, [COD]_t$ are the COD values corresponding to samples at the initial and t-time of oxidation process. The influence of the EDTA amount on COD values was eliminated by the blank sample in the same condition but without TNR.
Results and Discussion

*The reductive reaction of TNR by ZVI particles*

In near neutral medium, there is spontaneous iron oxidation with the production of hydrogen ions as shown in reaction 8.

$$2 \text{Fe}^{(0)} + 3 \text{H}_2\text{O} \rightarrow \text{Fe}_2\text{O}_3 + 6\text{e}^- + 6\text{H}^+ \quad (8)$$

When this half reaction is combined with reduction of TNR, the hydrogen ions are typically neutralized. The final reaction is given:

$$\text{C}_6\text{H}_3(\text{OH})(\text{NO}_2)_3 + 3 \text{H}_2\text{O} + 6 \text{Fe} \rightarrow \text{C}_6\text{H}_3(\text{OH})_2(\text{NH}_2)_3 + 3 \text{Fe}_2\text{O}_3.$$ 

In these conditions, the reduction of TNR by ZVI after 60 minutes was nearly complete. The reaction solutions become turbid due to the appearance of Fe$_2$O$_3$. After complete disappearance of TNR in the aqueous phase, ZVI is recovered and subjected to extraction with n-heptane. HPLC analysis of heptane extract indicated that there is no TNR in it. Reductive reaction of TNR carried out with dissolved ZVI does not result in TNR disappearance from the bulk solution. These finding indicate that (i) the observed TNR disappearance from bulk aqueous phase could be attributed to physical adsorption onto ZVI, and (ii) the TNR reduction can be attributed to chemical reactions mediated by iron surface.

![Graph](image-url)

**Fig.1 The change of TNR relative concentrations $\frac{C(TNR)_t}{C(TNR)_0}$ by ZVI**

Series 1, 2 and 3 are initial TNR concentration at 80mg/L, 100mg/L and 140mg/L respectively. The concentrations of TNR existed in suspense and adsorbed on iron surface (not presented here) were small, and neglected.
After every interval of 30 minutes, the concentrations of TNR in solutions were extracted by n-heptan and analyzed by HPLC method. The changes of TNR concentrations in solution (soluble) versus the reaction time are presented in Fig. 1.

Fig.1 indicates that with the increase of TNR concentrations (from 80mg/L to 140mg/L) the reaction rates between TNR and ZVI decrease. This was because of an influence of the initial concentrations of nitro aromatic compounds reacting with ZVI particle which has been reported by [3]. According to these authors, the highest reaction rate (k₁) corresponds to the lowest initial TNR concentration and the lowest k₁ corresponds to the highest initial TNR concentration. These results indicate that the reaction rate is a strong function of the number of surface active sites and therefore the ZVI:TNR molar ratio is an important reaction variable. During the reaction, the number of surface active sites decreases that causes the decrease of reaction rate. At the initial time of reaction, the number of surface active sites is high, at this moment, the reductive reaction rate of the TNR depends only on the initial TNR concentration. This means that the reaction kinetic order is pseudo-first one. The expression of reaction rate is as follows:

\[
\frac{d[TNR]}{dt} = -k_1[TNR], \quad (2).
\]

The data in Fig.1 show that when the number of surface active sites have decreased, the reaction rates in the reactions of series 1, 2, 3 decrease significantly after 60, 45 and 40 minutes respectively, when the number of surface active sites have decreased, the reaction rates decrease significantly. It means that at these times the reaction rates depend not only on the TNR concentrations but on the active surface sites of ZVI particles. The expression of these reaction rates corresponding to that times could be given as follows:

\[
\frac{d[TNR]}{dt} = -k_2[TNR][ZVI]. \quad (3).
\]

In this case, the reduction of TNR follows a second order rate law with respect to the TNR and iron concentrations.

Comparing (2) and (3), we have \( k_1 = k_2[ZVI] \). \( (4) \)

Based on the kinetic curves of the reductive reactions between TNR and ZVI, the \( k_1 \) would be determined and then \( k_2 \) value would be determined from \( k_1 \), by the expression \( k_2 = \frac{k_1}{[ZVI]} \). In this case, the \( k_1 = 0.015 \text{ mn}^{-1} \), \( k_2 = 0.022 \text{ M}^{-1}\text{L.mm}^{-1} \) have been determined.

**Oxidative reaction of the reduced products of TNR by ZVI particles**

The obtained amine products (in near 250 ml) from reductive reaction of TNR were mixed with other ZVI particles (10g) and 84mg of EDTA in a flask of 500 ml, in presence of oxygen from air. The efficiency of oxidative reaction of amine products by ZVI particles from our experiments was presented in Fig.2.
Fig. 2 The efficiency of oxidation reaction with ZVI particles in the presence of EDTA and oxygen

Series 1. The oxidation of amine products of the amine resorcine by ZVI.

Series 2. The direct oxidation of TNR by ZVI.

The experimental data showed that the efficiency of oxidative reaction of amine products by ZVI in the studied system was much higher than the direct oxidation of TNR. After 80 minutes of experiments the oxidative efficiency of amine resorcine achieved 98%, while direct oxidation of TNR was 28%. The oxidation of amine resorcine or TNR compound was implemented by the free radical \( \cdot OH \) generated in the system (see relations from 6 to 11). The easy oxidation of amine resorcine than TNR may be explicated by the attack of free radical \( \cdot OH \) on amine resorcine is more easy than on nitro resorcine. Some parameters such as the concentrations of TNR, ZVI, EDTA, pH solution influenced on the oxidative efficiency may become the subjects of the further studies.

The suggested treatment model of TNR contaminated groundwater

The treatment model of TNR contaminated groundwater consists of two units given in Fig 3. Water from well pumped into unit (I), where the polluted TNR compound is reduced; the polluted TNR compound is reduced by ZVI, form amine resorcine and \( Fe_2O_3 \). The amine products after a certain time will flow in the second unit for the oxidation step, where there is EDTA, sand, gravel and oxygen from air. The oxidation reaction between the amine resorcine and the free radical \( \cdot OH \) generated in the system will be carried out. The water come out from second unit will go to other treatment. After certain time both two units must be reactivated by a suitable diluted acid solution to remove the \( Fe_2O_3 \) layers on ZVI particles. The suggested model was applied to treat the TNR contaminated groundwater in a
military plant with the capacity of 5 m$^3$/day. The TNR concentration in groundwater was decreased from 35 ppm to 0.005 ppm. The system works normally, after every two weeks the system is reactivated by HCl diluted acid of 0.02M.

Fig. 3 The treatment model of TNR contaminated groundwater

(I) Unit containing ZVI and sand gravel.
(II) Unit containing ZVI, EDTA, sand saturated by oxygen.

Conclusion

The reduction of TNR by ZVI in anaerobic conditions and the oxidative reaction of amine resorcine in the system of ZVI-EDTA-O$_2$ have been very important for studying to remove TNR from groundwater. TNR compound can be reduced in the anaerobic conditions by ZVI and then its products would easily be oxidized in aerobic conditions in the system of ZVI-EDTA-O$_2$. HPLC method and analysis COD have been used for monitoring efficiency of reactions. From the obtained results, a model for TNR contaminated groundwater treatment has been suggested and successfully demonstrated.

References